

Power System Engineering
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Lecture – 54
Load frequency control (Contd.)

So, we have we have seen then this one.

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Where

$$\rightarrow \Delta P_{tie12} = \frac{|V_1||V_2|\cos(\delta_1^0 - \delta_2^0)}{x_{12}} (\Delta\delta_1 - \Delta\delta_2) \dots (22)$$

$$\rightarrow \therefore \frac{\Delta P_{tie12}}{P_{r1}} = \frac{|V_1||V_2|\cos(\delta_1^0 - \delta_2^0)}{P_{r1} x_{12}} (\Delta\delta_1 - \Delta\delta_2)$$

$$\rightarrow \therefore \Delta P_{tie12} (pu) = T_{12} (\Delta\delta_1 - \Delta\delta_2) \dots (23)$$

That both side we are dividing it by that your rated capacity of area-1 it is in megawatt right P r 1 is in megawatt, right. So, if you do so, then this will be in per unit. So, delta P tie 1 2 per unit is equal to T 1 2 delta delta 1 minus delta delta 2 this is equation-23.

One thing before proceeding further I would like to tell that hence onwards I mean after this equation-23 again and again we will not write per unit p u. We will simply write delta P tie 1 2, but it is understandable that all this quantities are in per unit values. So, now, T 1 2 actually is equal to magnitude V 1 magnitude V 2 cosine of delta 1 0 minus delta 2 0 divided by P r 1, x 1 2 right.

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Where

$$\rightarrow T_{12} = \frac{|V_1||V_2| \cos(\delta_1 - \delta_2)}{P_{r1} x_{12}}$$

Eqn. (23) can also be written as

$$\rightarrow \therefore \Delta P_{tie12} = 2\pi T_{12} \left[\int \Delta F_1 dt - \int \Delta F_2 dt \right] \dots (24)$$

ΔF_1 and ΔF_2 are frequency deviations in area-1 and area-2 respectively.

$$\dot{\delta} = \omega = 2\pi F$$

$$\therefore \dot{\delta}_1 = \omega_1$$

$$\therefore \Delta \dot{\delta}_1 = \Delta \omega_1 = 2\pi(\Delta F_1)$$

$$\Rightarrow \Delta \delta_1 = 2\pi \int \Delta F_1 dt$$

$$\Rightarrow \Delta \delta_2 = 2\pi \int \Delta F_2 dt$$

So, where T_{12} I have written here that magnitude V_1 magnitude V_2 cosine $\delta_1 - \delta_2$ upon P_{r1} into x_{12} . Now, there equation-23 can also be written as; that means, this equation-it can be written as your ΔP_{tie12} is equal to $2\pi T_{12}$ and $\Delta \delta_1$ and $\Delta \delta_2$ can be written as your 2π then T_{12} then integral of $\Delta F_1 dt$ minus integral of $\Delta F_2 dt$, this is equation-24.

How things are coming in general you know that $\dot{\delta}$ is equal to ω here I have done in for you is equal to $2\pi F$; F is the nominal frequency $2\pi F$ right. Now, therefore, say this is general thing $\dot{\delta}$. So, for δ_1 , so, $\dot{\delta}_1$ will be ω_1 ; that means, if I take small perturbation then $\Delta \dot{\delta}_1$ will be $\Delta \omega_1$ is equal to 2π it will be your ΔF_1 therefore, $\Delta \delta_1$; that means, if you integrate $\Delta \dot{\delta}_1$ will be 2π integral of $F \Delta F_1 dt$.

Similarly, here $\Delta \delta_2$ will be 2π integral of $\Delta F_2 dt$ that is why in this equation-that; that means, $\Delta \delta_1$ in this equation-you substitute 2π integral of $\Delta F_1 dt$ and here you substitute 2π integral of $\Delta F_2 dt$ take 2π common. So, it will become $2\pi T_{12}$. So, ΔP_{tie12} is equal to $2\pi T_{12}$ integral of $\Delta F_1 dt$ minus $\Delta F_2 dt$ this is equation-24, where ΔF_1 and ΔF_2 are frequency deviation in area one and area-2 respectively if there is a change in the load in either of the areas or in both the areas right.

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Similarly power flowing from area-2 to area-1
 can be given as:

$$\rightarrow \Delta P_{tie21} = 2\pi T_{21} \left[\int \Delta F_2 dt - \int \Delta F_1 dt \right] \dots (25)$$

Where

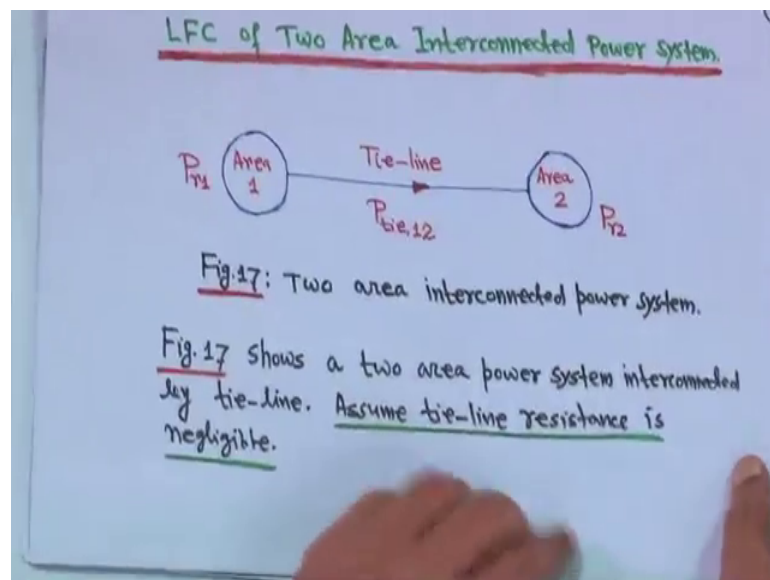
$$\rightarrow T_{21} = \frac{|V_2| |V_1| \cos(\delta_2 - \delta_1)}{P_{r2} X_{12}}$$

Eqn.(24) \div Eqn.(25)

$$\rightarrow \frac{\Delta P_{tie12}}{\Delta P_{tie21}} = -\frac{P_{r2}}{P_{r1}} = -\frac{1}{a_{12}} \quad \left[\because a_{12} = \frac{-P_{r1}}{P_{r2}} = \text{Area capacity Ratio} \right]$$

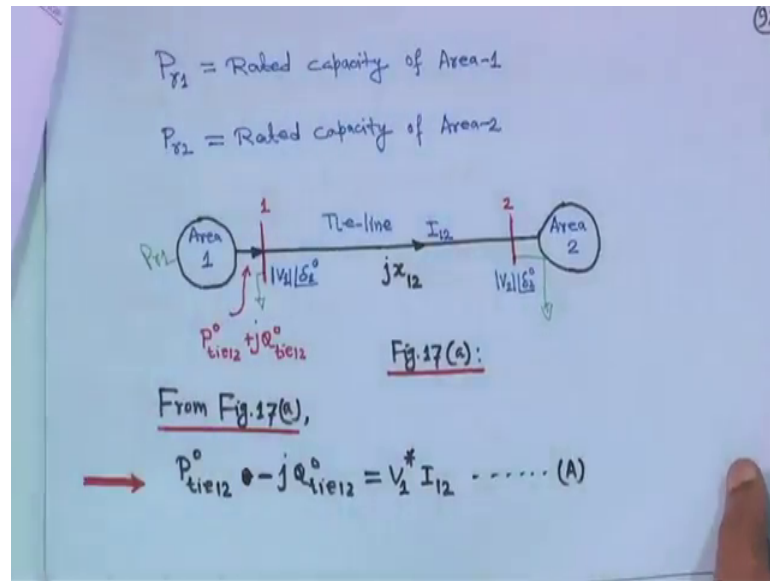
Therefore, similarly power flowing from area-2 to area-1, this is I am not doing from this inspection you can write power flowing from area-2 to area-1.

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That means, from this side to that side if you take here direction is showing that 1 to 2.

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That means if power flows in this direction from 2 to 1 in this direction then you can directly write $\Delta P_{tie 21}$ is equal to $2\pi T_{21} \int \Delta F_2 dt - \int \Delta F_1 dt$ right. So, in this case it is 1 2 and in this case just interchange those suffix it will be $\Delta P_{tie 21}$ it will be $2\pi T_{12}$ right T 2 sorry $2\pi T_{21}$ and it will be become integral of ΔF_2 minus integral of $\Delta F_1 dt$; So, just, just opposite to that.

Therefore, $\Delta P_{tie 21}$ is equal to $2\pi T_{21} \int \Delta F_2 dt - \int \Delta F_1 dt$. Basically, basically if you look into the diagram if you look into the diagram because line resistance is neglected there is. So, here if it is $\Delta P_{tie 21}$, 1 2 rather and in this side if it is $\Delta P_{tie 21}$ then in real unit when it is in megawatt basically $\Delta P_{tie 12}$ is equal to minus of $\Delta P_{tie 21}$ because loss is neglected. So, everywhere this deviation will remain same, we are not considering the power loss right.

Therefore, this equation-similarly we can write, but in, but where ΔT_{21} this one V_2 , V_1 same thing cosine earlier it was $\cos \delta_1 - \cos \delta_2$ you know. So, earlier it was $\cos \delta_1 - \cos \delta_2$, now it is $\cos \delta_2 - \cos \delta_1$ same thing divided by x_{12} , but it is in area-2 that is why divided by the rated capacity P_{r2} , right. So, this is your divided by P_{r2} .

Previous one that it was in area one that is why it was divided by your P_{r1} both side. So, that means, this is in per unit I will I told you that I will not mention again and again,

but this is in per unit delta. So, T_{21} is this one, right. Therefore, if divide equation-24 by equation-25, that means, your this is 24. So, divide equation-24 by equation-25; that means, this one; that means, this one. So, if you do. So, you will get ΔP_{tie12} upon ΔP_{tie21} you just do it know you will get it. It is nothing, but minus P_{r2} upon P_{r1} is equal to say we are writing one upon a 1 2, right.

That means a 1 2 is equal to minus P_{r1} upon P_{r2} we will call area capacity ratio, but minus sign is taken care of. If you if you do not take minus sign here then block diagram that will change with that minus a 1 2, right, otherwise if you take a 1 2 is equal to minus P_{r1} upon P_{r2} actually P_{r1} upon P_{r2} is area capacity ratio, but with this minus sign sometimes we call this is also area capacity ratio. So, this is actually it is written 1 upon a 1 2. So, once it is done that your what you call this ratio therefore, your $T_{\Delta P_{tie21}}$ is equal to a 1 2 into ΔP_{tie12} .

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$\rightarrow \Delta P_{tie21} = a_{12} \Delta P_{tie12} \dots (26)$

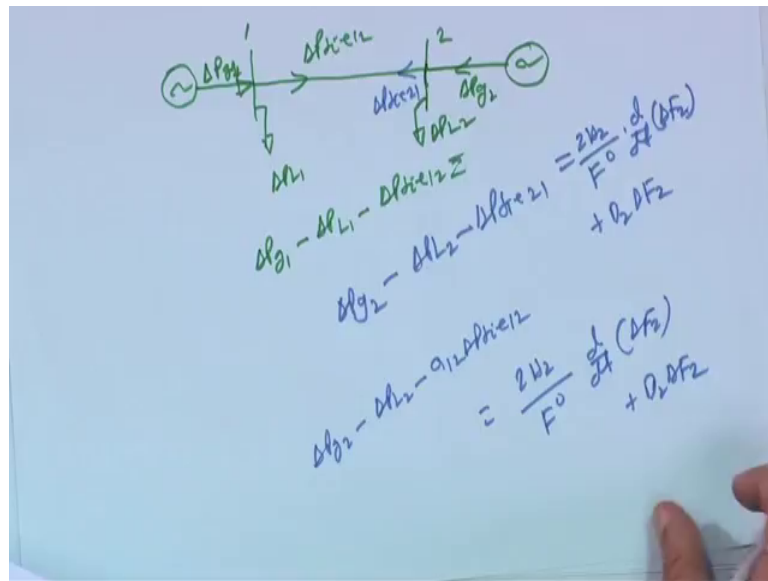
With reference to Eqn(10), incremental power balance equation for area-1 can be written as:

$\rightarrow \Delta P_{g1} - \Delta P_{L1} - \Delta P_{tie12} = \frac{2H_1}{F^0} \frac{d(\Delta F_1)}{dt} + D_1 \Delta F_1 \quad \left[\begin{array}{l} F^0 = f^0 \\ \Delta F_1 = \Delta f_1 \end{array} \right] \dots (27)$

So, that is why this ΔP_{tie21} is equal to a 1 2 into ΔP_{tie12} in generally if you take a real unit I mean in megawatt forget about that that suppose it is not a it is not a per unit values. So, if it is a megawatt then if and if a 1 2 is minus 1 actually because ΔP_{tie21} will be minus of ΔP_{tie12} because loss is neglected. So, at any point of the line this power you will remain same because loss we have neglected.

So, now with reference to equation-10 incremental power balance equation-for area one can be written as we have seen earlier you know just have a look this one.

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Suppose, suppose you have a generator suppose you have a generator is suppose giving power say P_{g1} and this is your load say it is we are writing your ΔP_{L1} and generation power also change say ΔP_{g1} and this is the tie line connected that. So, this is your power this is 1 and this side is 2. So, this is your ΔP_{tie12} then what is the power balance equation here? $\Delta P_{g1} - \Delta P_{L1} - \Delta P_{tie12}$ is equal to during because of the load disturbance; that means, transient in balance between generational load hence that will hence the tie power also it will be affected.

So, if you if you just write down the power balance equation, so, $\Delta P_{g1} - \Delta P_{L1} - \Delta P_{tie12}$ is same as before $2H_1$ this area-1. So, we have taken H_1 is the inertia constant $2H_1$ upon F_0 then $\frac{d}{dt}$ of ΔF_1 plus $D_1 \Delta F_1$. This F_0 and small f_0 superscript is this thing same. Similarly, ΔF_1 capital ΔF_1 and Δf_1 , they are same actually right. So, this is the equation-during transient imbalance. We will see later, but at steady state what will happen this term will vanish this term will vanish. Because, a steady state derivative is 0 only this term will exist that will see later.

So, therefore, at during transient imbalance so, $\Delta P_{g1} - \Delta P_{L1}$ because at steady state if you write the equation-at steady state then ΔP_{g1} is equal to actually $\Delta P_{L1} + \Delta P_{tie12}$ right, but we if you take the difference this is at and this will happen during transient imbalance. So, it will be your $2H_1 F_0 \frac{d}{dt} \Delta F_1$

same thing we have seen further single area system detail have been given for isolated case plus $D_1 \Delta F_1$. This is for area one that is why you are putting ΔF_1 $d_1 H_1$; H_1 is the inertia constant. So, this is actually equation-27, right.

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(102)

Taking Laplace transform of Eqn. 27) and reorganizing, we get,

$$\rightarrow \Delta F_1 = \left[\Delta P_{g1} - \Delta P_{L1} - \Delta P_{tie12} \right] \times \frac{K_{p1}}{1 + sT_{p1}} \dots (28)$$

Where

$$\rightarrow K_{p1} = \frac{1}{D_1}; T_{p1} = \frac{2H_1}{D_1 F_0} \dots (29)$$

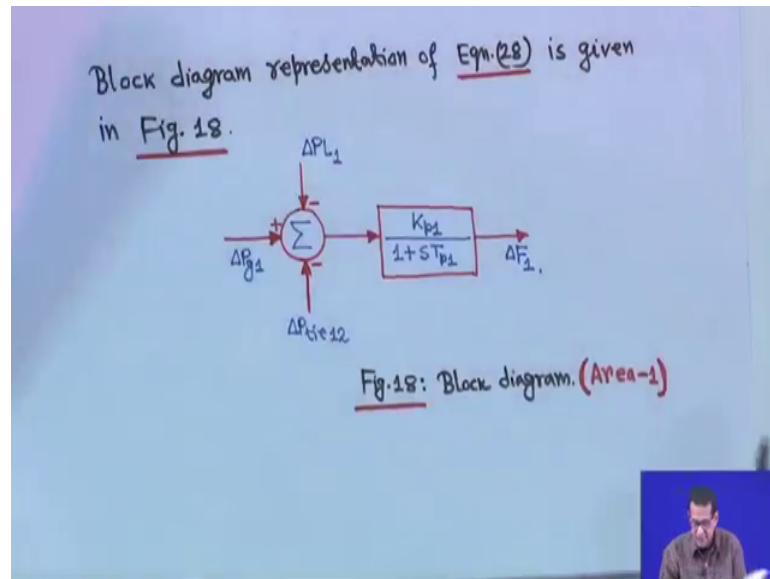
So, next is that if you take the Laplace transform on both side of this equation-this equation-again and again not putting ΔP_{g1} s or ΔP_{tie12} , yes, it is understandable. If you take the Laplace transform same as before and just simplify, just simplify, right. So, what will get ΔF_1 will get ΔP_{g1} minus ΔP_{L1} minus ΔP_{tie12} we are not putting again and again all this thing in a function of S because it is understandable into K_{p1} upon $1 + sT_{p1}$ this is equation-28. Actually for the isolated system ΔP_{tie} was not there rest was same here also ΔP_{tie} is there, that is why minus ΔP_{tie12} into the same thing earlier for isolated case it was K_{p1} upon $1 + sT_{p1}$.

Now, it is for area-1 that is why it is into K_{p1} upon one plus sT_{p1} , right; that means, where K_{p1} is equal to 1 upon D_1 we know that K_{p1} is equal to 1 upon D_1 for isolated case we have seen for area-1 K_{p1} is equal to 1 upon D_1 similarly for isolated case we have seen $2H_1$ upon $d_1 F_0$ it is for area-1 that is why T_{p1} is equal to $2H_1$ upon $D_1 F_0$, right. So, this is your what you call that equation- related to ΔF_1 ΔP_{g1} ΔP_{L1} and ΔP_{tie12} this is equation-28 and this two we are marking as equation-29.

So, this is understandable right you take the Laplace transverse same as the isolated case only one tau added here that is because interconnection that delta P tie 1 2, right.

So, once this is done just hold on. So, once this is done then the block for this thing if you try to replace and it is your block diagram this one.

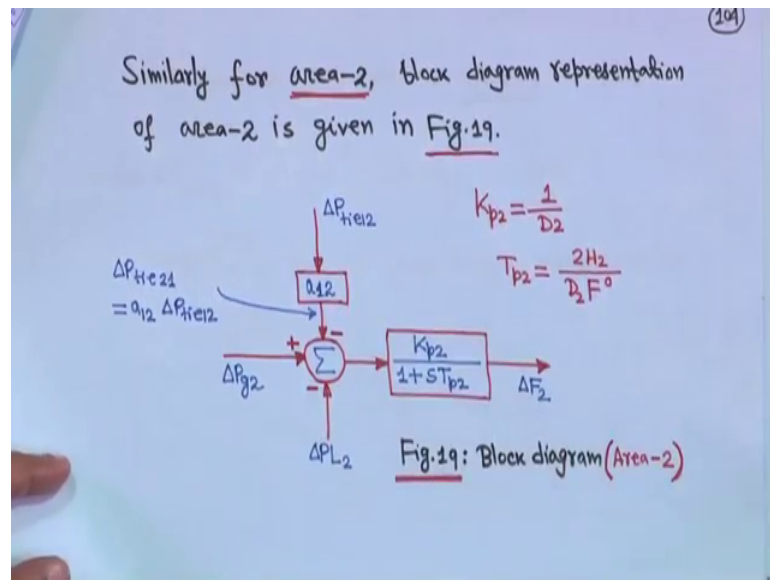
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So, you can write this is delta P g 1 this is plus right delta P g 1 minus delta P L 1 minus delta P tie 1 2. So, this is minus delta P L 1 and this is say it is coming from somewhere will see later it is minus delta P tie 1 2 then into K p 1 upon 1 1 plus S T p 1 and output is that delta F 1 this is actually block diagram for area-1 this is actually only power your what you call this power system part right, power system and tie line part and later we will later and this generation also later will see from where it is coming when you will do for area-2 so, and the complete block diagram.

So, this is this equation-this equation-equation 28 actually is represented by this block diagram that is written here that block diagram representation of equation-20 is given in figure 18 this is figure 18 , right.

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Next is next is similarly, for area-2 block diagram representation of area-2 is give given in figure 19 this 1 in the figure 2 what will happen that you know sorry in area-2 it will be K_{p2} upon $1 + s T_{b2}$ ΔP_{g2} will be there minus ΔP_{tie12} and this is your minus $a_{12} \Delta P_{tie12}$, how things are coming here right, this a_{12} because this is actually ΔP_{tie21} .

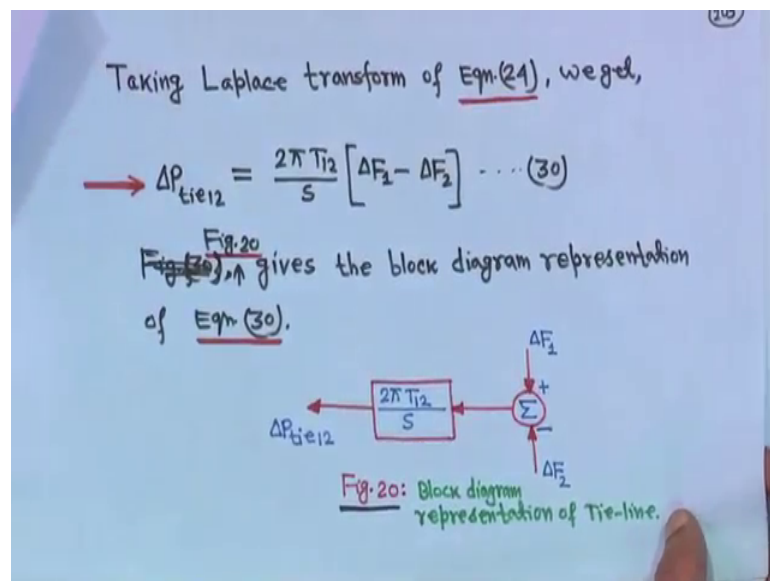
So, if you consider area-2 say this area if you consider here see here I am I am simply making it here only if this is your generator area-1. So, this power due to say that ΔP_{g2} and this is your ΔP_{L2} right and this side ΔP_{tie12} and this direction if you make it is ΔP_{tie21} loss is neglected; that means, power balance equation-actually same way will get $\Delta P_{g2} - \Delta P_{L2} - \Delta P_{tie21}$ is equal to your this equation you will get that if power during power imbalance that is this 1 this 1 you can write like this that is your $2 H_2$ divided by your F_0 into $d dt$ of your ΔF_2 plus D_2 into ΔF_2 , right.

And, and another thing is that as we have seen that ΔP_{tie21} is equal to $a_{12} \Delta P_{tie12}$ tie your what you call a_{12} . So, here if you substitute this one then it will become $\Delta P_{g2} - \Delta P_{L2} - a_{12} \Delta P_{tie12}$ because ΔP_{tie21} is equal to $a_{12} \Delta P_{tie12}$, right from equation-26 is equal to the same thing $2 H_2$ upon F_0 , F_0 is a nominal system frequency then $d dt$ then ΔF_2 plus $D_2 \Delta F_2$, right. So, this is for area-2 this is for area 2.

Now, if you again take the Laplace transform you will get the your what you call the same thing only the delta P tie that instead of your K p 1 T p 1 it will be your K p 2 upon T p 2 1 plus S T p 2 and this is actually delta P tie 2 1 that is actually is equal to a 1 2 into delta P tie 1 2, right, that we have seeing that is why it is coming it block diagram is made like this and a 1 2 is equal to minus P r 1 upon P r 2. So, that it is written here so, and this is delta P g 2 and this minus delta P 2.

So, this is K p 2 upon 1 plus S T p 2 that is delta F 2 this is actually figure-19 this is block diagram portion of area 2. So, this is this is power system this is tie power we will see from where it is coming and this is delta P g 2 and this is minus delta your minus delta P 2, right. So, in this case I mean in this case I mean very your what you call that next we have to complete the block diagram.

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So, what will do from that your from equation 24, right from this equation-24 if you come to this right or I am writing like this that equation-24 you are written like this know rather than searching I am writing here.

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The image shows a person's hands writing on a whiteboard. The text on the board is as follows:

$$\Delta P_{tie-1,2} = 2\pi T_{12} \left[\int \Delta F_1 dt - \int \Delta F_2 dt \right]$$

$$\Delta P_{tie-1,2} = 2\pi T_{12} \left[\frac{\Delta F_1}{s} - \frac{\Delta F_2}{s} \right]$$

$$= \frac{2\pi T_{12}}{s} [\Delta F_1 - \Delta F_2]$$

Below the equations, the text reads: "Taking Laplace transform". At the bottom, the final result is written as: $\Delta P = \frac{2\pi T_{12}}{s} [\Delta F_1 - \Delta F_2]$.

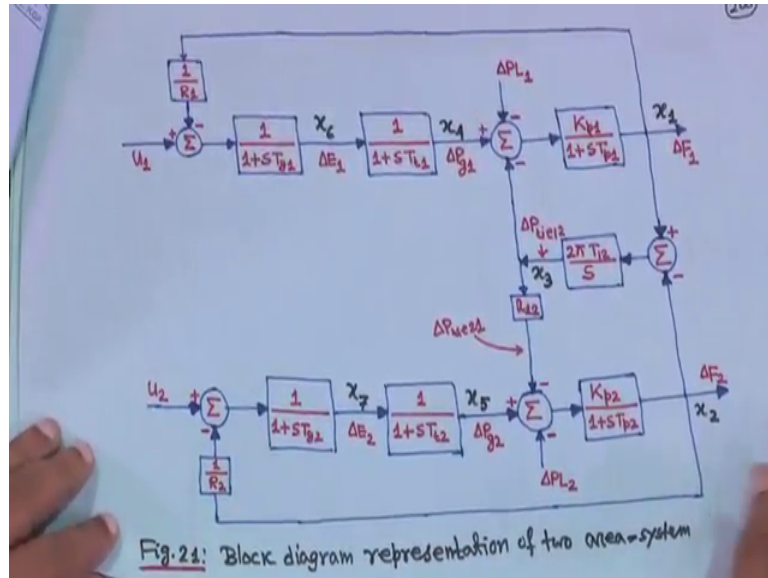
That $\Delta P_{tie-1,2}$ is equal to $2\pi T_{12}$ right in bracket it was integral of $\Delta F_1 dt$ minus integral of $\Delta F_2 dt$ right. So, if you take the Laplace transform then it will be $\Delta P_{tie-1,2}$ yes, I am not putting in bracket it is understandable right, is equal to $2\pi T_{12}$ right. So, this 1 in the bracket if you take the Laplace transform it will be ΔF_1 upon s minus ΔF_2 upon s right it is actually ΔF_1 function upon s ΔF_2 actually function upon s , but not putting. So, that mean this will be equal to $2\pi T_{12}$ upon s right in bracket it will be ΔF_1 minus ΔF_2 , right.

That means the tie line power equation-also can be represented in terms of Laplace transform right. So, the that is why we are writing ΔP that is taking the this actually this was actually your equation-24 this was actually equation-24 just previously you have seen. So, so $\Delta P_{tie-1,2}$ we can write $2\pi T_{12} \Delta F_1$ minus $2\pi T_{12}$ upon s ΔF_1 minus ΔF_2 this is equation-thirty if for this equation-block diagram if you make then this is $\Delta P_{tie-1,2}$ is equal to $2\pi T_{12}$ upon s into ΔF_1 minus ΔF_2 this is the block diagram representation of the tie line; that means, the tie line also can be modelled in the s domain right.

So, this is the tie line power equation. So, now, if you if you complete the block diagram now; that means, this tie this $\Delta P_{tie-1,2}$ whatever we have seen whatever we have seen in the previous block diagram this $\Delta P_{tie-1,2}$ right, actually this is your $\Delta P_{tie-1,2}$ this is $\Delta P_{tie-1,2}$ here also $\Delta P_{tie-1,2}$, right and this $\Delta P_{tie-1,2}$ you have

to connect from here from this equation-from this delta P tie 1 2 here. now, if you make the complete block diagram of two area system, right then it will be like this.

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So, if you look into this then this is your area-1, this is the control signal u_1 this is for isolated system you have seen ΔF was coming to 1 upon r then minus feedback here, right. But, here it is area one. So, ΔF_1 is coming here 1 upon r this is this is for non reheat turbine only right because if I try to put 1 more block per reheat I cannot accommodate here and this is your $1 \text{ upon } 1 \text{ plus } S T t_1$ this is $\Delta P g_1$ and this is your disturbance 1 this is $K p_1 \text{ upon } 1 \text{ plus } S T p_1$ this is ΔF_1 .

Similarly, here this is u_2 the control signal this is ΔF_2 it is $1 \text{ upon } r_2$, $1 \text{ upon } 1 \text{ upon } 1 \text{ plus } S T g_2$ $1 \text{ upon } 1 \text{ plus } S T t_2$ $\Delta P g_2$ this is disturbance minus ΔP_2 and this is this is ΔF_2 . So, just now we have seen now $\Delta P_{tie 1 2}$ is equal to $2 \pi T_{12} \text{ upon } S \Delta F_1 \text{ minus } \Delta F_2$, this 1 we have seen now $\Delta P_{tie 1 2}$ is equal to this one. So, this is the block this is the block. So, $\Delta P_{tie 1 2}$ is equal to $2 \pi T_{12} \text{ upon } S \Delta F_1 \text{ minus } \Delta F_2$. So, this $\Delta P_{tie 1 2}$ we have seen now $\Delta P g_1 \text{ minus } \Delta P_1 \text{ minus } \Delta P_{tie 1 2}$, right your whatever we have seen into $K p_1 \text{ upon } S \text{ plus } T p_1$ ΔF_1 .

Similarly, here also we have seen know this is $\Delta P_{tie 1}$ this we have also you have seen know that previous block diagram that this one modelling actually. So, this block diagram we have seen know this one same thing we have same thing it is here only here

also same thing here also. So, this is delta P tie 1 2, but delta P tie 2 1 is equal to a 1 2 delta P tie 1 2, right. So, it is minus. So, delta P g 2 minus delta and this is K p 2 upon 1 plus S T p 2 and this is your delta F 2, right.

So, this a two area interconnected system block diagram. Assuming that in each area there is one unit if you have more unit like composite modelling then you have to put. So, many; now, for the classroom purpose I think I call the classroom purpose this is ok, right. So, this is control signal later we will see that. Now, question is that we have to put then in the state variable form that is x dot is equal to a x plus b u plus gamma P.

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From Fig. 21, state-variable equations can be written as:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \\ \dot{x}_5 \\ \dot{x}_6 \\ \dot{x}_7 \end{bmatrix} = \begin{bmatrix} -\frac{1}{T_{p1}} & 0 & -\frac{K_{p1}}{T_{p1}} & \frac{K_{p2}}{T_{p1}} & 0 & 0 & 0 \\ 0 & -\frac{1}{T_{p2}} & -\frac{K_{p2}}{T_{p2}} & 0 & \frac{K_{p1}}{T_{p2}} & 0 & 0 \\ 2\pi T_{12} & -2\pi T_{12} & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\frac{1}{T_{e1}} & 0 & \frac{1}{T_{e2}} & 0 \\ 0 & 0 & 0 & 0 & -\frac{1}{T_{e2}} & 0 & \frac{1}{T_{e1}} \\ -\frac{1}{R_1 T_{g1}} & 0 & 0 & 0 & 0 & \frac{1}{T_{g2}} & 0 \\ 0 & -\frac{1}{R_2 T_{g2}} & 0 & 0 & 0 & 0 & \frac{1}{T_{g1}} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \\ x_7 \end{bmatrix}$$

Now, I have written everything all this things for you, but let me write down all another thing is that the state variable is marked it is arbitrary. Actually whatever here you want it is arbitrary it does not matter result will remain same, but here frequency is x 1 that delta F 1 that is why we have made x 1 because our interest will be generally frequencies and tie power, right I mean generation also.

So, that is why the delta F 1 is mark as x 1 delta F 2 is given as a state variable x 2 and tie power it is given state variable x 3 this we have written generation 1 written as x 4 and generation 2 written as a x 5 and as here it is x 6 is delta E 1 and your just governor output right something and it this there is a these are the quantity not directly measurable and this is your delta E 2 is given x 7.

So, system is actually there are and if you look into that there are two disturbance your element there $\Delta P L 1$ and $\Delta P L 2$ and two control signals are there $u u 1$ and $u 2$ and there are 7 such blocks are there you representing your Laplace transform your S represent a term is; that means, this system order is 7 into a matrix will be 7 into 7 and 2 us are there $u 1$ and $u 2$, two control signals are there ; that means, b matrix will be 7 into 2 and disturbance 1 $\Delta P L 1$ and $\Delta P L 2$.

So, disturbance matrix will be 7 into 2. So, when will write this equation- just I am writing for all of you this thing first you take the $x 1$, right. So, if you all the everything is written here, but I will show you how we are making it.

So, if you take the $x 1$ first this 1 first then it will be I am making it here when will I am making from here only when will see this recording thing you will just write down on your note notebook first this one and then make one by one, right.

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$$x_1 = \frac{k_{p1}}{(1+sT_{p1})} [x_1 - x_3 - \Delta PL_1]$$

$$\therefore x_1 + (sT_{p1})T_{p1} = -k_{p1} \cdot x_3 + k_{p2} \cdot x_4 - k_{p2} \cdot \Delta PL_1$$

$$\therefore x_1 T_{p1} = -x_1 - k_{p2} \cdot x_3 + k_{p2} \cdot x_4 - k_{p2} \cdot \Delta PL_1$$

$$\therefore x_1 = \frac{-1}{T_{p1}} x_1 - \frac{k_{p1}}{T_{p1}} x_3 + \frac{k_{p2}}{T_{p1}} x_4 - \frac{k_{p2}}{T_{p1}} \Delta PL_1$$

So, when we write $x 1$ look $x 1$ is equal to right it is $K p 1$ upon 1 plus $S T p 1$ right then in bracket it will be $x 4$ right it will be $x 4$. So, it is $x 4$ then minus this is actually $x 3$. So, this is also $x 3$.

So, minus $x 3$ right and this is minus $\Delta P L 1$ this is $\Delta P L 1$. So, $x 4$ is equal to $K P 1$ into 1 plus $S T P 1$ then your $x 4$ minus $x 3$ minus $\Delta P L 1$; that means, if you go for cross multiplication then it is $x 1$ plus $S x 1$ into $T p 1$ is equal to this $x 3$ I am writing

first minus K_{p1} into x_3 plus K_{p1} into x_4 , right minus K_{p1} into ΔPL_1 , right. That means, this $S \times 1$ is actually $x_1 \dot{S}$ mean all initial conditions are 0, $x_1 \dot{T}$ this x_1 is going to the right hand side minus x_1 minus $K_{p1} x_3$ right then your plus K_{p1} into x_4 minus K_{p1} into ΔPL_1 .

That means your $x_1 \dot{S}$ is equal to minus 1 upon it is T_{p1} upon T_{p1} then x_1 minus your K_{p1} upon T_{p1} this is x_3 plus K_{p1} upon T_{p1} x_4 right minus K_{p1} upon T_{p1} ΔPL_1 . So, this is this is that your first equation $x_1 \dot{S}$ is equal to. So, x_1 term is there x_3 is there x_4 is there other state variables are not there and ΔPL_1 is there; that means, in this equation in this equation if you see that $x_1 \dot{S}$ is equal to minus 1 upon T_{p1} into x_1 it is minus 1 upon T_{p1} into x_1 then x_2 is not there.

So, it is 0 then minus K_{p1} upon T_{p1} into x_3 minus K_{p1} upon T_{p1} into x_3 , right, plus your K_{p1} T_{p1} into x_4 plus K_{p1} T_{p1} into x_4 right no other x are involve. So, all 0, 0, 0 then it is my disturbance matrix first element minus K_{p1} upon your T_{p1} minus K_{p1} upon T_{p1} into ΔPL_1 it is in the next page right u is not involve. So, u is not involved.

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$$\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{1}{T_{p2}} & 0 \\ 0 & \frac{1}{T_{p2}} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} + \begin{bmatrix} -\frac{K_{p2}}{T_{p2}} & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} -\frac{K_{p2}}{T_{p2}} & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \Delta PL_1 \\ \Delta PL_1 \end{bmatrix} \dots (31)$$

So, here first row it is 0 0 and it is first one if ΔPL_1 minus $K_{p1} T_{p1}$ first equation-into ΔPL_1 second is not there, so, it is 0. This is first equation- right. So, similarly if you take the your what you call second one second one such that you will not

be your what you call you will not be confused or anything, you can easily make it of your own.

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$$x_2 = \frac{k_{p2}}{(1 + sT_{p2})} [x_5 - a_{12}x_3 - d_{PL2}]$$

$$\therefore x_2 + (s x_2) T_{p2} = k_{p2} x_5 - a_{12} x_3 - d_{PL2}$$

$$\therefore \dot{x}_2 T_{p2} = -x_2 - \frac{k_{p2}}{a_{12}} x_3 + k_{p2} x_5 - d_{PL2}$$

$$\therefore \dot{x}_2 = -\frac{1}{T_{p2}} x_2 - \frac{k_{p2} a_{12}}{T_{p2}} x_3 + \frac{k_{p2}}{T_{p2}} x_5 - \frac{d_{PL2}}{T_{p2}}$$

$$\therefore \dot{x}_2 = -\frac{1}{T_{p2}} x_2 - \frac{k_{p2} a_{12}}{T_{p2}} x_3 + \frac{k_{p2}}{T_{p2}} x_5 - \frac{d_{PL2}}{T_{p2}}$$

Now, second one what will do if you look into that this equation then we can write x_2 is equal to we can write x_2 is equal to K_{p2} upon $1 + S T_{p2}$ then in bracket then it is x_5 it is x_5 , right. So, this is x_5 then minus now, this is x_3 . So, here d_{PL2} will be actually a $1/2$ into x_3 because it this is $x_3 \times 3$ into a $1/2$ here it is a $1/2 \times 3$ that is d_{PL2} .

So, minus your a $1/2$ into x_3 this 1 right then disturbance is that d_{PL2} minus d_{PL2} now, if you go for cross multiplication if you go for cross multiplication it is x_2 plus $S x_2 T_{p2}$ is equal to $K_{p2} x_5$ minus $a_{12} x_3$ minus d_{PL2} , right ; that means, $S x_2$ is x_2 dot so, x_2 dot T_{p2} this x_2 taking this side minus x_2 then this is writing first x_3 a $1/2 \times 3$ then plus $K_{p2} x_5$ minus d_{PL2} .

That means x_2 dot is equal to minus 1 upon $T_{p2} \times 2$ minus a_{12} upon $T_{p2} \times 3$ plus K_{p2} upon $T_{p2} \times 5$ minus 1 upon $T_{p2} d_{PL2}$ sorry here that multiplication of K_{p2} I have missed it, here it should be K_{p2} , right. A multiplication here also it will be your multiplied by K_{p2} here also it will be multiplied by K_{p2} I have missed it; that means, here it will be K_{p2} into a $1/2$, right and here also it will be K_{p2} your in your K_{p2} into x_5 right, minus your a $1/2 K_{p2}$ into x_3 minus here I have also missed it will be K_{p2} into d_{PL2} , right; So, this 1 also K_{p2} into d_{PL2} .

So, rewriting in a in a phase once again x_2 is equal to $\frac{-1}{T_p^2} x_2 - \frac{K_p}{2a} \frac{1}{T_p^2} x_3$ right, then plus $\frac{K_p}{2} \frac{1}{T_p^2} x_5 - \frac{K_p}{2} \frac{1}{T_p^2} \Delta P L^2$, right. So, this is that this is the equation- right here actually at the time of multiplication I have missed this 1 right.

So, question is that now this is the now you check this equation equation-2 you check. So, there is no in this equation if you look into that here no x_1 is involve. So, second equation is 0. Next is $\frac{-1}{T_p^2} x_2$. So, $\frac{-1}{T_p^2}$ then, x_3 if you look $\frac{-1}{2} \frac{K_p}{T_p^2} x_2 - \frac{1}{2} \frac{K_p}{T_p^2} x_2$, x_4 is not there 0, x_5 is there x_5 is this one, right $\frac{K_p}{2} \frac{1}{T_p^2}$ right and then your this then the other state variables are not there.

So, it is 0 0 and if you go to the then no u is involve only the disturbance in area-2 is involved no u is involved here therefore, it is 0 0 and here it is 0 and it is $-\frac{K_p}{2} \frac{1}{T_p^2} \Delta P L^2$. So, this is the second equation.

Thank you we will be.