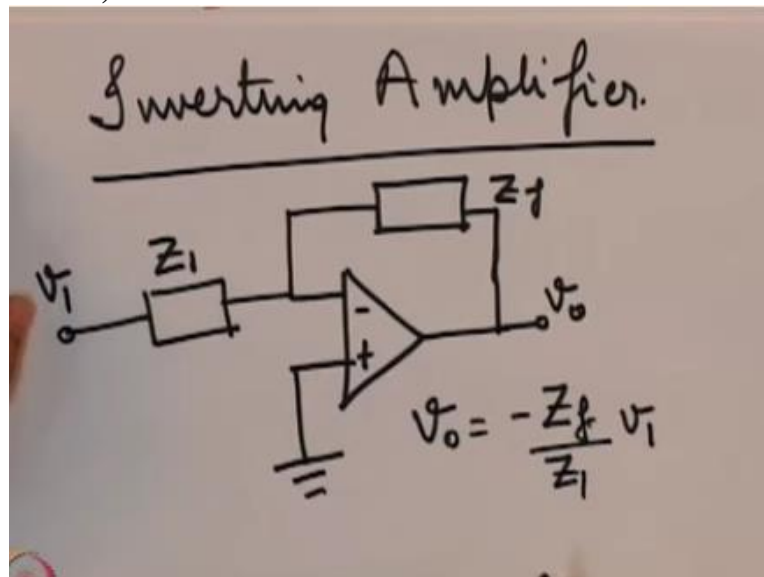


Analog Circuits
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Week -01
Module -05
Inverting amplifier and Non-inverting amplifier

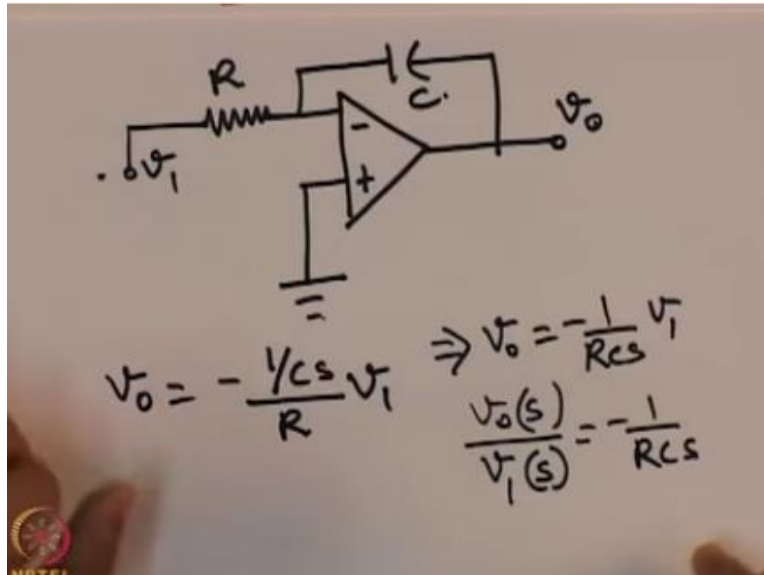
Welcome to another module of this course analog circuits. In the last module we had talked about the inverting amplifier and the summer inverter amplifier and then I had also introduced you to the formula for any general inverting amplifier with general impedances.

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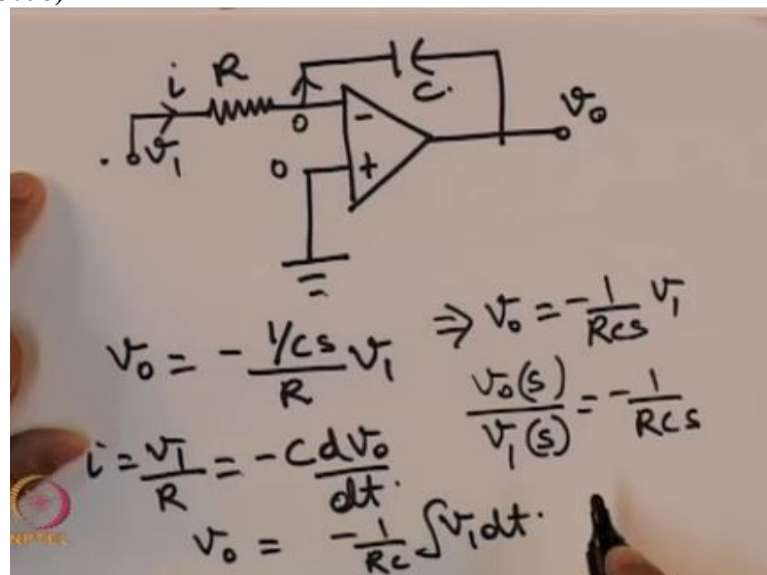
Here we shall be using that formula to further discuss some of the other circuits, so once again if we can write the formula for the general inverting amplifier with general impedances not just resistances, so this is the formula letting the output voltage v_0 to v_1 suppose our Z_1 and Z_f are like this.

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Of course, we can simply analyze this as v_0 is equal to -1 upon CS upon $R v_1$ which implies v_0 is equal to 1 upon Rcs upon v_1 now this is a low pass transfer function, if we can write a transfer function of the system it is v_0 upon v_1 upon Rcs , as we can see this is a low pass transfer function, because as s tends to infinity the value of the magnitude of this transfer function keeps decreasing, but in order to also see the time domain response let us try to write the time domain equations.

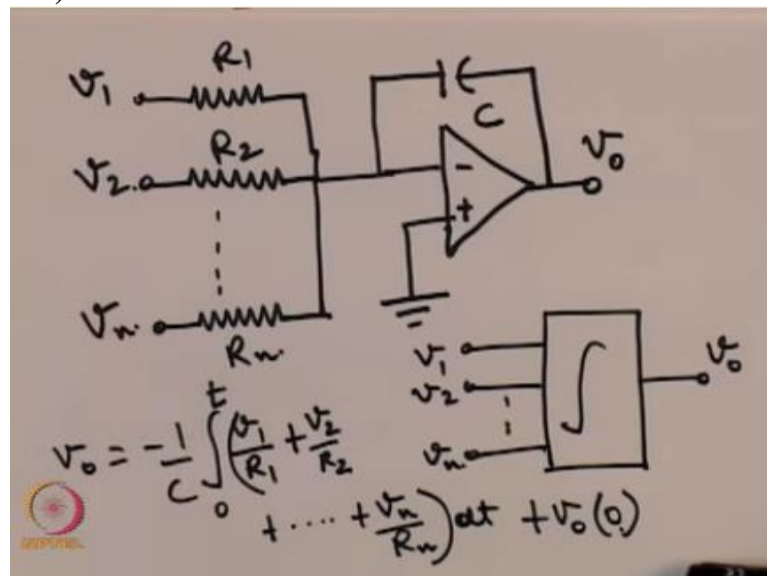
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So once again you see that these 2 terminals are at 0 voltage is a virtual short between the inverting and non-inverting terminals and so I can write the current i is again flowing only through $i R$ and C the current i flowing through R can be written as i is equal to v_1 upon R and the current flowing through C is $-C dv_0$ upon dt .

So then v_0 is equal to -1 upon $RC \int v_1 dt$ so this is an integrator the circuit is an integrator which also matches with the transfer function because I mean the transfer function of an integrator is always a low pass filter prototype this is also an inverting integrator okay because there is this negative sign at the beginning if we in place just like the summer inverter or summer inverting amplifier if we have a series of in input voltages which are connected at the input not just one input then the circuit becomes something like this and my V_0 .

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So this is the block diagram of this integrator or summer integrator and the output Voltage in time domain is given as you where this v_0 at 0 is the initial condition so this is the formula for integrator now just like the non-inverting or the inverting amplifier we also have to take into account the currents that are flowing so just like the previous case suppose we have a limitation on the maximum current that can be supplied.

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$$|i_{max}| = \left| C \frac{dv_o}{dt} + I_L \right| < C \cdot$$

\downarrow
 max value of
 OPAMP O/P current

$$C \frac{dv_o}{dt} = - \left(\frac{v_1}{R_1} + \frac{v_2}{R_2} + \dots + \frac{v_n}{R_n} \right)$$

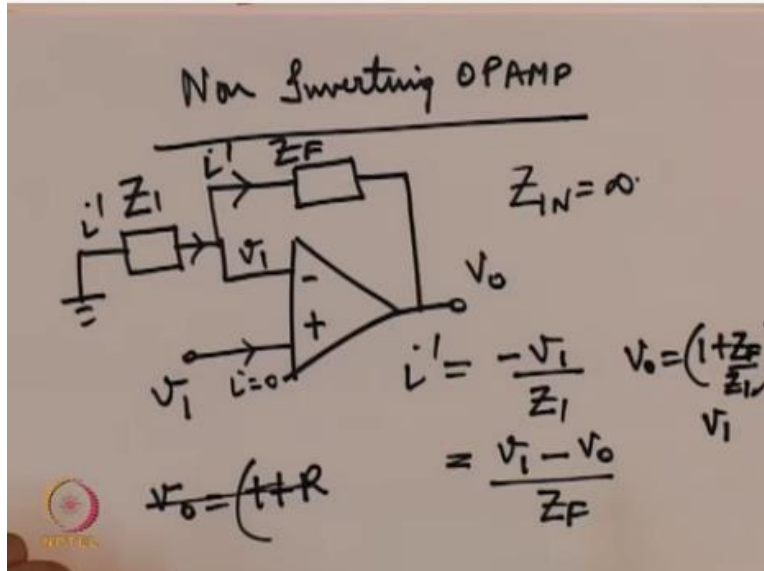
$$\left| I_L - \left(\frac{v_1}{R_1} + \frac{v_2}{R_2} + \dots + \frac{v_n}{R_n} \right) \right| < C \cdot$$

So suppose if we go back to this inverter itself and suppose the maximum current that can be supplied and the output is I_{max} was the current going to the load is I_L , then what is the current flowing through this capacitor a current flowing through this capacitor is simply given by $C \frac{dv_o}{dt}$ upon dt in this direction, if you consider the current flowing in this direction then of course it will be there will be a negative sign.

So this current is $C \frac{dv_o}{dt}$ upon dt okay the current flowing through the load is I_L so I_{max} is equal to $C \frac{dv_o}{dt} + I_L$ and this whole thing should be lesser than some value C maximum value of opamp output current so using this equation, we can find out a value of I_L or the maximum current or the minimum current that can be always supplied by.

So what we do is we can find out what is the worst value of the $C \frac{dv_o}{dt}$ upon dt and based on that we can find out the minimum I_L that will always be supplied instead of attempting to calculate the $C \frac{dv_o}{dt}$ both 0 upon dt we note that $C \frac{dv_o}{dt}$ upon dt is equal to $-\left(\frac{v_1}{R_1} + \frac{v_2}{R_2} + \dots + \frac{v_n}{R_n} \right)$. For this formula, can be reduced as okay next we go on to the other opamp configuration which is called the non-inverting configuration.

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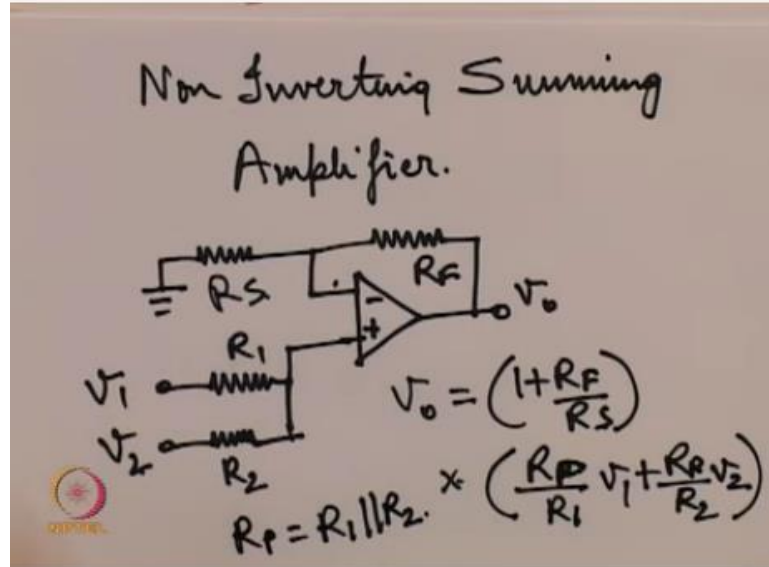
So we had an inverting configuration now we have a non-inverting configuration so the non-inverting configuration so the non-inverting opamp, now let us try to derive the relationship between v_1 and v_0 again we note that the current flowing in the non-inverting terminal will be 0 because the input impedance of the opamp is very high therefore for a non-inverting opamp Z_{in} will be equal to infinity.

Next let us try to see the relationship between v_0 and v_1 , now since this 2 terminals non-inverting and non-inverting terminals are at virtual shot and since the non-inverting terminal is connected to v_1 and we can say that because of this virtual shot the inverting terminal will also be at v_1 , then what is the current flowing to the through this Z_1 .

So we can say suppose I call that i_1 you can say i_1 is equal to $-v_1$ upon Z_1 and since no component of i_1 will flow inside the inverting terminal all i_1 will flow through Z_F , therefore I can also write this i_1 in terms of Z_F as $v_1 - v_0$ upon Z_F now equating the 2 we will see that V_0 will be given by $1 + R$ or sorry let me V_0 is equal to $1 + Z_F$ upon Z_1 times V_1 .

I leave the calculation for the output impedance of this configuration as an exercise for you let us see whether we can obtain a similar summing configuration like we obtained for the inverting of them for this non-inverting case also we need a circuit for non-inverting summing amplifier.

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So, we have suppose we have 2 inputs like this we can show that this output V_0 will equal to $1 + \frac{R_F}{R_S}$ times $\frac{R_P}{R_1} V_1 + \frac{R_P}{R_2} V_2$ where this R_P is equal to R_1 parallel to R_2 in fact for a number of such sources when in here we have considered only 2 inputs.

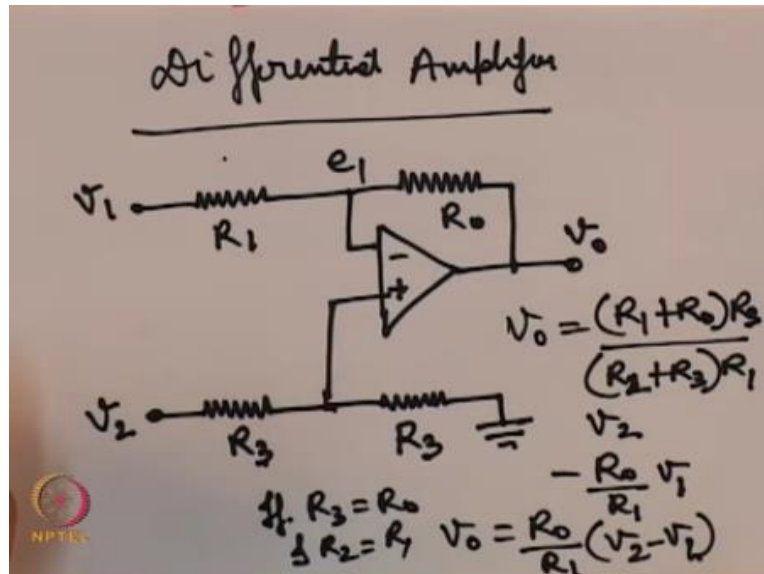
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$$V_o = \left(1 + \frac{R_F}{R_S}\right) \times \left(\frac{R_P}{R_1} V_1 + \frac{R_P}{R_2} V_2 + \dots + \frac{R_P}{R_n} V_n\right)$$

$$R_P = R_1 \parallel R_2 \parallel \dots \parallel R_n$$

But suppose we have more than 2 input then this V_0 is given by $1 + \frac{R_F}{R_S}$ multiplied by R_P times $\frac{V_1}{R_1} + \frac{V_2}{R_2} + \dots + \frac{V_n}{R_n}$ where this R_P is equal to R_1 parallel to R_2 till R_n , now taking this concept or rather combining both the inverting and non-inverting configurations in the same circuit we obtain what is known as a differential amplifier.

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So here this is a combination of both the inverting and non-inverting opamp, if only v_1 is present and v_2 is not present then by virtue of this short this point will also be shortened, which basically means that there is this R_3 plays no role because the current here is 0.

So in that case the output will simply be equal to an non-inverting, the whole opamp will act like and inverting opamp and if only v_2 is present and v_1 is not present then it has it acts like a non-inverting opamp, now you can prove that (()) (17:47) overall impact of this whole circuit will be something like a differential amplifier and actually the output will be given by this formula if R_3 is equal to R_0 and R_2 is equal to R_1 then v_0 will be equal to R_0 upon R_1 times $v_2 - v_1$, now here what you see is that this output is directly proportional to the difference between v_1 v_2 and v_1 so that is why this term it is called a differential amplifier.

It produces an output which is proportional to the difference between the 2 inputs only unlike the previous cases for the non-inverting and inverting cases where only the input v_1 and v_2 were individually amplified for a differential amplifier, the output is proportional to the difference between the 2 and then one other use of an opamp is implementation of a transfer function, so this we have already seen briefly.

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$$V_o = -Z_F(s)$$

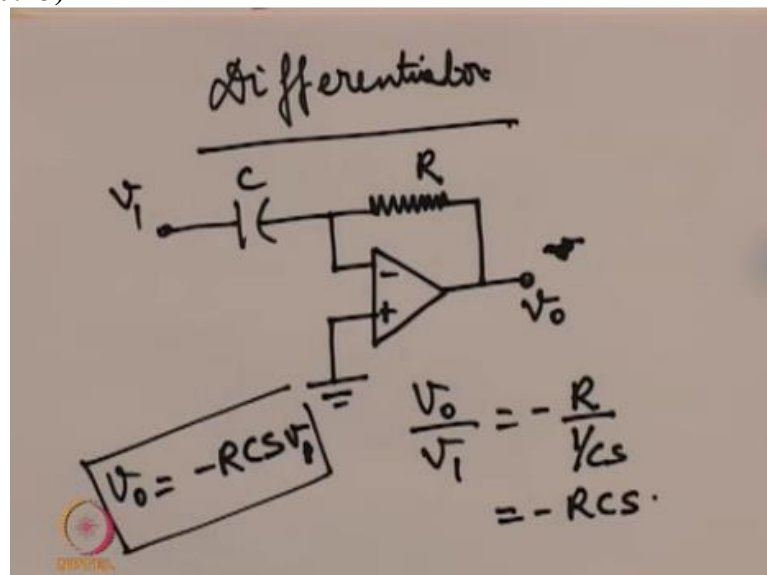
feedback impedance

$$V_o = \frac{-Z_F(s)}{Z_I(s)}$$

feedback impedance

Because for an opamp V_o is given by $-Z_F$ this Z_F is also known as the feedback impedance by the feedback impedance that is why we use the subscript F, let me write it correctly now depending what we choose as Z_F+Z_I we can implement the appropriate transfer function one other circuit that we can also implement using a opamp and which follows naturally from an integrator is the differentiator if we can implement and integrate a non opamp then we should also be able to implement a differentiator.

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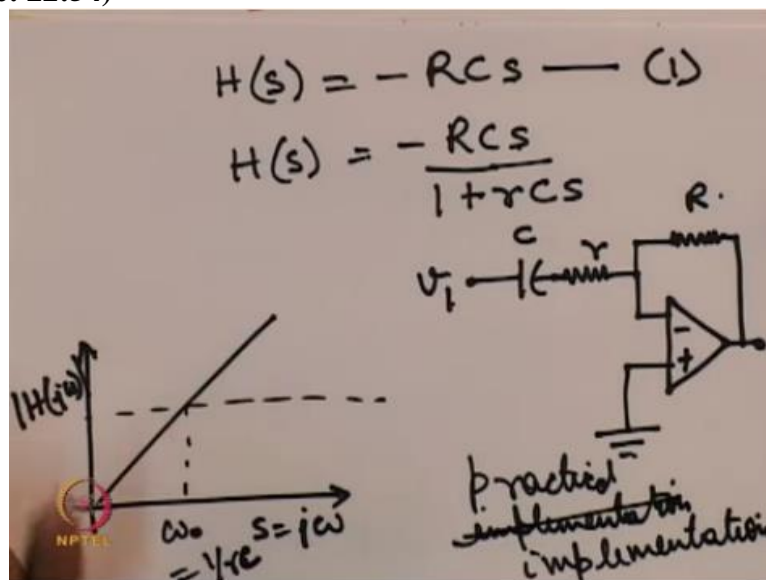


So in all this differentiator so in all these discussions that we had so far you see that we are using the opamp for various operations like summing than integration difference differential operation then finally differentiation so a simple way of implementing a differentiator might be this you

know just the reverse of what we did for an invert integrator the problem with this kind of implementation is that when the input is or the frequency is 0.

Let us see what happens so we have v_0 is equal to $-RCS v_1$ at S equal to 0 the magnitude of the transfer function becomes 0 and therefore that becomes a problem, so this is a differentiator circuit whose transfer function is given by this equation, now here we see that as the frequency increases that is as the value of S increases the output keeps on blowing up or it becomes very high and that is not really desirable.

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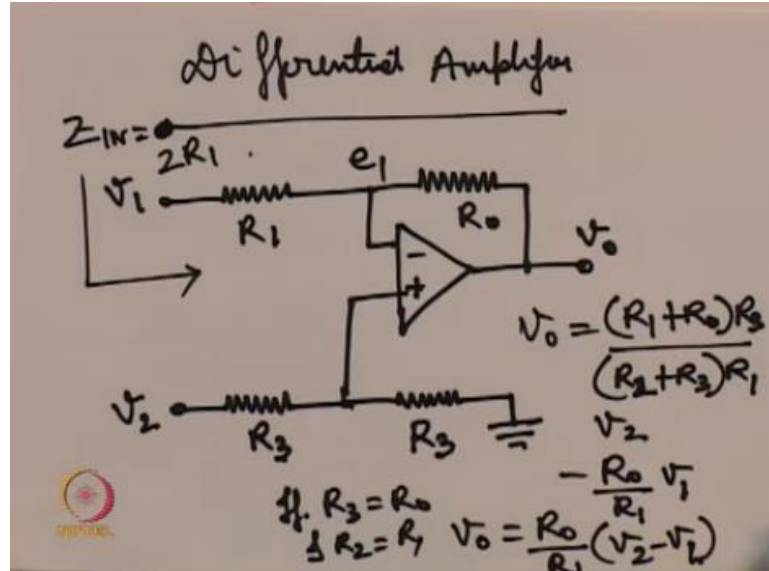
So instead of that, if we have a implementation with a transfer function like this $H(s)$, so in this case if I write in our case $H(s)$ is or the transfer function is equal to RCS let us label it as equation 1 and if we try to plot this magnitude of $H(s)$ with ω or we take S equal to $J\omega$ and this as H of $J\omega$

Then we see that when our transfer function is like this then it simply blows up like this so instead of this if we have a transfer function which does not blow up at infinity at S equal to infinity but is something like this so in this case what we get is the circuit for implementing such a transfer function will be like this ok.

So we purposely introduced a resistance small resistance are in series which will create instead of this transfer function blowing up, if we plot the asymptotic plot of H of $J\omega$ then at a

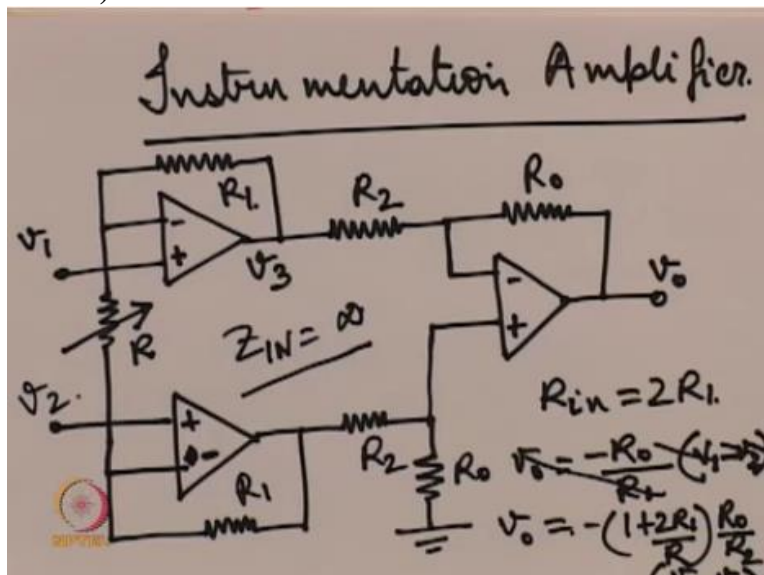
certain frequency $\omega \rightarrow 0$ given by $\frac{1}{\omega RC}$ small R capital C at this frequency instead of the transfer function going on along a straight line it will asymptotically the transfer function will become flat, so this is a more practical implementation.

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So one problem with the differential amplifier is that the input impedance Z_{in} is equal to $2R_1$, it can be you know you can find it out you can calculate this and find out that the Z_{in} is indeed equal to $2R_1$, now for many applications we need a high input impedance as we had discussed earlier for a Voltage amplifier the input impedance should be always very high, but in this case it is not so high and that is disadvantage so in place of a differential amplifier we sometimes use what is known as an instrumentation amplifier.

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So an instrumentation amplifier has a circuit like this, now since in this case the V_1 and V_2 are supplied directly to the non-inverting terminal of 2 opamps the input impedance is equal to infinity and the output Voltage is given by this equation, it is still the output is still proportional to the difference between the inputs but the only difference is not the only difference of course the circuit is now consumes has more number of components more number of opamps and therefore it consumes more power.

But still the main advantage of this instrumentation amplifier is the input impedance which is now very high and necessary for a Voltage amplifier. So with this we covered most of the topics that were there with an opamp we have covered the basics of the inverting opamp the basics of the non-inverting opamp and we shall still be covering as we proceed along this course a wide variety of opamp circuits.

But in the next lecture or the next module, we shall be introducing some concepts of non idealities that are present in an opamp and how they are characterized and how they affect the performance of the circuit and how they can be reminded, thank you.